

ON OPTIMIZATION OF MANUFACTURING PLANAR DOUBLE-BASE HETEROTRANSISTORS TO DECREASE THEIR DIMENSIONS

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ABSTRACT

In this paper we consider an approach of manufacturing of double-base heterotransistors to decrease their dimensions. Framework the approach it should be manufactured a heterostructure with specific configuration. Farther it is necessary to dope certain areas of the heterostructure by diffusion or by ion implantation. After finishing of the doping process the dopant and/or radiation defects should be annealed. We consider an approach of optimization of dopant and/or radiation defects for manufacturing more compact double-base heterotransistors.

KEYWORDS

Field-effect heterotransistors; double-base heterotransistors; increasing of integration rate

1. INTRODUCTION

Development of the solid state electronic devices leads to necessity to decrease dimensions of elements of integrated circuits, to increase their performance and reliability. One way to increase performance of the solid state electronic devices is searching materials with higher charge carriers mobility [1-3]. Another way to increase the performance is development of new or optimization of existing technological processes [4-7]. To increase reliability of the solid state electronic devices are could be also used development of new or optimization of existing technological processes [4-7]. One way to decrease dimensions of elements of integrated circuits is using laser or microwave types of annealing [8-10]. Using these types of annealing leads to generation inhomogenous distribution of temperature. The inhomogeneity with account Arrhenius law leads to inhomogeneity of dopant and radiation defects diffusion coefficients and another parameters. The inhomogeneity of parameters gives us possibility to decrease dimensions of elements of integrated circuits. Properties of materials could be also changed by using radiation processing [11,12].

In this paper we consider a heterostructure, which consist of a substrate and epitaxial layer (see Figs. 1). The epitaxial layer includes into itself several sections, which manufactured by using another materials (see Figs. 1). The sections should be doped by diffusion or by ion implantation to generation required type of conductivity (n or p). We assume, that another area of epitaxial layer has reverse type of conductivity (p or n). We also assume, that substrate is insulator. Farther we consider annealing dopant and /or radiation defects. Increasing of annealing time leads to in-

creasing of diffusion length into nearest materials. Decreasing of annealing time did not lead to full doping of sections of the epitaxial layer. Main aim of the present paper is choosing compromise value of annealing time.

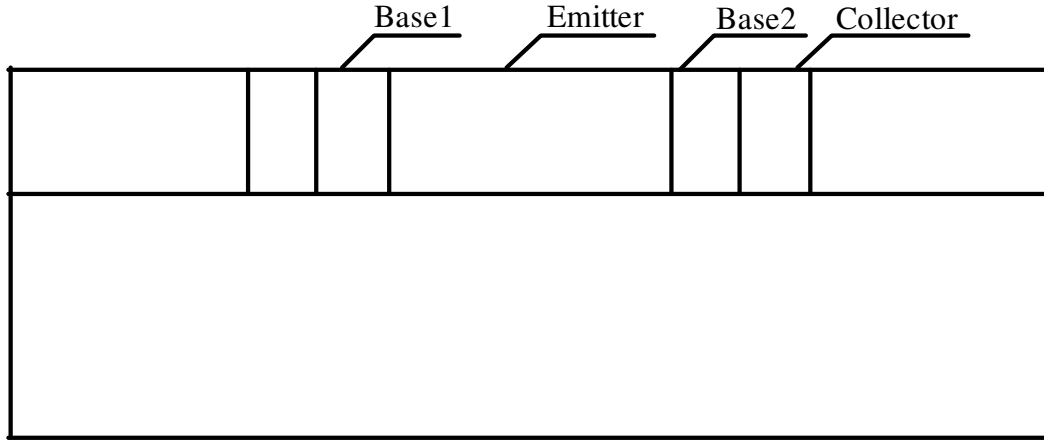


Fig. 1a. Heterostructure which consist of a substrate and a multisectional epitaxial layer. Side view

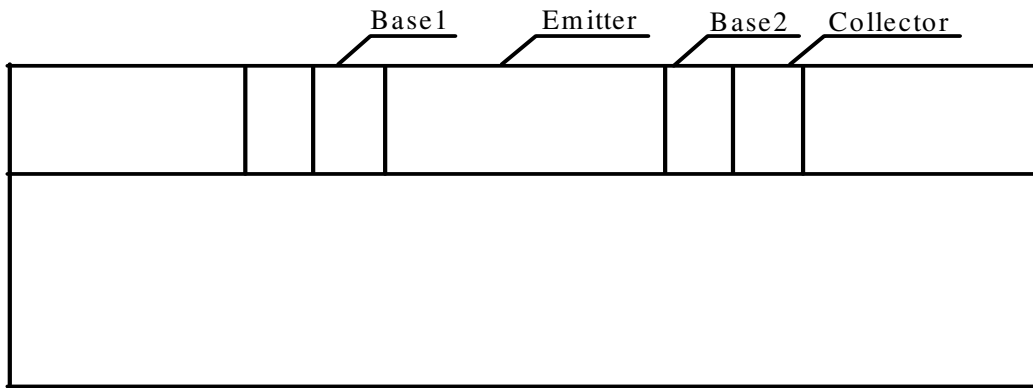


Fig. 1b. Heterostructure which consist of a substrate and a multisectional epitaxial layer. Top view

2. METHOD OF SOLUTION

To achieve our aim we determine spatio-temporal distributions of concentrations of dopant and radiation defects. We determine the required distribution of concentrations of dopant by solution of the following boundary problem

$$\frac{\partial C(x, y, z, t)}{\partial t} = \frac{\partial}{\partial x} \left[D_c \frac{\partial C(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_c \frac{\partial C(x, y, z, t)}{\partial y} \right] + \frac{\partial}{\partial z} \left[D_c \frac{\partial C(x, y, z, t)}{\partial z} \right]. \quad (1)$$

$$\left. \frac{\partial C(x, y, z, t)}{\partial x} \right|_{x=0} = 0, \quad \left. \frac{\partial C(x, y, z, t)}{\partial x} \right|_{x=L_x} = 0, \quad \left. \frac{\partial C(x, y, z, t)}{\partial y} \right|_{y=0} = 0, \quad \left. \frac{\partial C(x, y, z, t)}{\partial y} \right|_{x=L_y} = 0,$$

$$\left. \frac{\partial C(x, y, z, t)}{\partial z} \right|_{z=0} = 0, \quad \left. \frac{\partial C(x, y, z, t)}{\partial z} \right|_{x=L_z} = 0, \quad C(x, y, z, 0) = f(x, y, z). \quad (2)$$

Here $C(x,y,z,t)$ is the spatio-temporal distribution of concentration of dopant; T is the temperature of annealing; D_C is the dopant diffusion coefficient. Value of dopant diffusion coefficient depends on properties of materials of heterostructure, speed of heating and cooling of heterostructure (with account Arrhenius law). Dependences of dopant diffusion coefficient on parameters could be approximated by the following relation [12-14]

$$D_C = D_L(x, y, z, T) \left[1 + \xi \frac{C^\gamma(x, y, z, t)}{P^\gamma(x, y, z, T)} \right] \left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right]. \quad (3)$$

where $D_L(x,y,z,T)$ is the spatial (due to presents several layers in heterostructure) and temperature (due to Arrhenius law) dependences of dopant diffusion coefficient; $P(x,y,z,T)$ is the limit of solubility of dopant; parameter γ depends on properties of materials and could be integer in the following interval $\gamma \in [1,3]$ [13]; $V(x,y,z,t)$ is the spatio-temporal distribution of concentration of radiation vacancies; V^* is the equilibrium distribution of concentration of vacancies. Concentrational dependence of dopant diffusion coefficient has been described in details in [13]. It should be noted, that using diffusion type of doping did not generation radiation defects. In this situation $\zeta_1 = \zeta_2 = 0$. We determine spatio-temporal distributions of concentrations of radiation defects by solving the following boundary problem [12,14]

$$\begin{aligned} \frac{\partial I(x, y, z, t)}{\partial t} = & \frac{\partial}{\partial x} \left[D_I(x, y, z, T) \frac{\partial I(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_I(x, y, z, T) \frac{\partial I(x, y, z, t)}{\partial y} \right] - k_{I,I}(x, y, z, T) \times \\ & \times I^2(x, y, z, t) + \frac{\partial}{\partial z} \left[D_I(x, y, z, T) \frac{\partial I(x, y, z, t)}{\partial z} \right] - k_{I,V}(x, y, z, T) I(x, y, z, t) V(x, y, z, t) \end{aligned} \quad (4)$$

$$\begin{aligned} \frac{\partial V(x, y, z, t)}{\partial t} = & \frac{\partial}{\partial x} \left[D_V(x, y, z, T) \frac{\partial V(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_V(x, y, z, T) \frac{\partial V(x, y, z, t)}{\partial y} \right] - k_{V,V}(x, y, z, T) \times \\ & \times V^2(x, y, z, t) + \frac{\partial}{\partial z} \left[D_V(x, y, z, T) \frac{\partial V(x, y, z, t)}{\partial z} \right] - k_{I,V}(x, y, z, T) I(x, y, z, t) V(x, y, z, t). \end{aligned}$$

Boundary and initial conditions for these equations are

$$\begin{aligned} \left. \frac{\partial \rho(x, y, z, t)}{\partial x} \right|_{x=0} = 0, \quad \left. \frac{\partial \rho(x, y, z, t)}{\partial x} \right|_{x=L_x} = 0, \quad \left. \frac{\partial \rho(x, y, z, t)}{\partial y} \right|_{y=0} = 0, \quad \left. \frac{\partial \rho(x, y, z, t)}{\partial y} \right|_{y=L_y} = 0, \\ \left. \frac{\partial \rho(x, y, z, t)}{\partial z} \right|_{z=0} = 0, \quad \left. \frac{\partial \rho(x, y, z, t)}{\partial z} \right|_{z=L_z} = 0, \quad \rho(x, y, z, 0) = f_\rho(x, y, z). \end{aligned} \quad (5)$$

Here $\rho=I,V$; $I(x,y,z,t)$ is the spatio-temporal distribution of concentration of radiation interstitials; $D_\rho(x,y,z,T)$ are the diffusion coefficients of point radiation defects; terms $V^2(x,y,z,t)$ and $I^2(x,y,z,t)$ correspond to generation divacancies and diinterstitials; $k_{I,V}(x,y,z,T)$ is the parameter of recombination of point radiation defects; $k_{I,I}(x,y,z,T)$ and $k_{V,V}(x,y,z,T)$ are the parameters of generation of simplest complexes of point radiation defects.

We determine spatio-temporal distributions of concentrations of divacancies $\Phi_I(x,y,z,t)$ and diinterstitials $\Phi_V(x,y,z,t)$ by solving the following boundary problem [12,14]

$$\begin{aligned} \frac{\partial \Phi_I(x,y,z,t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_I}(x,y,z,T) \frac{\partial \Phi_I(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{\Phi_I}(x,y,z,T) \frac{\partial \Phi_I(x,y,z,t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_{\Phi_I}(x,y,z,T) \frac{\partial \Phi_I(x,y,z,t)}{\partial z} \right] + k_{I,I}(x,y,z,T) I^2(x,y,z,t) - k_I(x,y,z,T) I(x,y,z,t) \end{aligned} \quad (6)$$

$$\begin{aligned} \frac{\partial \Phi_V(x,y,z,t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_V}(x,y,z,T) \frac{\partial \Phi_V(x,y,z,t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_{\Phi_V}(x,y,z,T) \frac{\partial \Phi_V(x,y,z,t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_{\Phi_V}(x,y,z,T) \frac{\partial \Phi_V(x,y,z,t)}{\partial z} \right] + k_{V,V}(x,y,z,T) V^2(x,y,z,t) - k_V(x,y,z,T) V(x,y,z,t), \\ \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial x} \right|_{x=0} &= 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial x} \right|_{x=L_x} = 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial y} \right|_{y=0} = 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial y} \right|_{y=L_y} = 0, \\ \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial z} \right|_{z=0} &= 0, \quad \left. \frac{\partial \Phi_\rho(x,y,z,t)}{\partial z} \right|_{z=L_z} = 0, \quad \Phi_I(x,y,z,0) = f_{\Phi_I}(x,y,z), \quad \Phi_V(x,y,z,0) = f_{\Phi_V}(x,y,z). \end{aligned} \quad (7)$$

Here $D_{\Phi_\rho}(x,y,z,T)$ are the diffusion coefficients of the above complexes of radiation defects; $k_I(x,y,z,T)$ and $k_V(x,y,z,T)$ are the parameters of decay of these complexes.

We determine spatio-temporal distribution of concentrations of dopant and radiation defects by method of averaging of function corrections [15] with decreasing quantity of iteration steps [16]. Framework the approach we used solutions of Eqs. (1), (4), (6) with averaged values of diffusion coefficients $D_{0L}, D_{0I}, D_{0V}, D_{0\Phi_I}, D_{0\Phi_V}$, zero values of parameters of recombination of radiation defects and parameters of generation and decay of their complexes as initial-order approximations of required concentrations. The initial-order approximations could be written as

$$\begin{aligned} C_1(x,y,z,t) &= \frac{1}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{nC} c_n(x) c_n(y) c_n(z) e_{nC}(t), \\ I_1(x,y,z,t) &= \frac{1}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{nI} c_n(x) c_n(y) c_n(z) e_{nI}(t), \\ V_1(x,y,z,t) &= \frac{1}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{nV} c_n(x) c_n(y) c_n(z) e_{nV}(t), \\ \Phi_{I1}(x,y,z,t) &= \frac{1}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{n\Phi_I} c_n(x) c_n(y) c_n(z) e_{n\Phi_I}(t), \\ \Phi_{V1}(x,y,z,t) &= \frac{1}{L_x L_y L_z} + \frac{2}{L_x L_y L_z} \sum_{n=1}^{\infty} F_{n\Phi_V} c_n(x) c_n(y) c_n(z) e_{n\Phi_V}(t), \end{aligned}$$

where $e_{n\rho}(t) = \exp\left[-\pi^2 n^2 D_{0\rho} t \left(\frac{1}{L_x^2} + \frac{1}{L_y^2} + \frac{1}{L_z^2}\right)\right]$, $F_{n\rho} = \int_0^{L_x} c_n(u) \int_0^{L_y} c_n(v) \int_0^{L_z} c_n(w) f_\rho(u, v, w) dw dv du$,
 $c_n(\chi) = \cos(\pi n \chi / L_\chi)$.

We determine approximations of the second-and higher-orders framework standard iteration procedure of method of averaging of function corrections [16,17]. Framework this procedure to determine the n -th-order approximation of concentrations of dopant and radiation defects we shall replace the required functions $C(x, y, z, t)$, $I(x, y, z, t)$, $V(x, y, z, t)$, $\Phi_I(x, y, z, t)$ and $\Phi_V(x, y, z, t)$ in the right sides of Eqs. (1), (4), (6) on the following sums $\alpha_{n\rho} + \rho_{n-1}(x, y, z, t)$, when $\alpha_{n\rho}$ are not yet known average values of the n -th-order approximation of the above concentrations. The replacement leads to the following relations for the second-order approximations of the required concentrations

$$\begin{aligned} \frac{\partial C_2(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_L(x, y, z, T) \left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right] \frac{\partial C_1(x, y, z, t)}{\partial x} \right] \times \\ &\times \left\{ 1 + \xi \frac{[\alpha_{2c} + C_1(x, y, z, t)]^\gamma}{P^\gamma(x, y, z, T)} \right\} + \frac{\partial}{\partial y} \left[D_L(x, y, z, T) \left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right] \right] \times \\ &\times \left\{ 1 + \xi \frac{[\alpha_{2c} + C_1(x, y, z, t)]^\gamma}{P^\gamma(x, y, z, T)} \right\} \frac{\partial C_1(x, y, z, t)}{\partial y} + \frac{\partial}{\partial z} \left\{ \left[1 + \xi \frac{[\alpha_{2c} + C_1(x, y, z, t)]^\gamma}{P^\gamma(x, y, z, T)} \right] \right\} \times \\ &\times D_L(x, y, z, T) \left[1 + \zeta_1 \frac{V(x, y, z, t)}{V^*} + \zeta_2 \frac{V^2(x, y, z, t)}{(V^*)^2} \right] \frac{\partial C_1(x, y, z, t)}{\partial z} \end{aligned} \quad (8)$$

$$\begin{aligned} \frac{\partial I_2(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_I(x, y, z, T) \frac{\partial I_1(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_I(x, y, z, T) \frac{\partial I_1(x, y, z, t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_I(x, y, z, T) \frac{\partial I_1(x, y, z, t)}{\partial z} \right] - k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, t)] [\alpha_{2V} + V_1(x, y, z, t)] - \\ &- k_{I,I}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, t)]^2 \end{aligned} \quad (9)$$

$$\begin{aligned} \frac{\partial V_2(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_V(x, y, z, T) \frac{\partial V_1(x, y, z, t)}{\partial x} \right] + \frac{\partial}{\partial y} \left[D_V(x, y, z, T) \frac{\partial V_1(x, y, z, t)}{\partial y} \right] + \\ &+ \frac{\partial}{\partial z} \left[D_V(x, y, z, T) \frac{\partial V_1(x, y, z, t)}{\partial z} \right] - k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, t)] [\alpha_{2V} + V_1(x, y, z, t)] - \\ &- k_{V,V}(x, y, z, T) [\alpha_{2V} + V_1(x, y, z, t)]^2 \end{aligned}$$

$$\begin{aligned} \frac{\partial \Phi_{I2}(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, t)}{\partial x} \right] + k_{I,I}(x, y, z, T) I^2(x, y, z, t) + \\ &+ \frac{\partial}{\partial y} \left[D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, t)}{\partial y} \right] + \frac{\partial}{\partial z} \left[D_{\Phi_I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, t)}{\partial z} \right] - \\ &- k_I(x, y, z, T) I(x, y, z, t) \end{aligned} \quad (10)$$

$$\begin{aligned} \frac{\partial \Phi_{v_2}(x, y, z, t)}{\partial t} &= \frac{\partial}{\partial x} \left[D_{\Phi v}(x, y, z, T) \frac{\partial \Phi_{v_1}(x, y, z, t)}{\partial x} \right] + k_{v,v}(x, y, z, T) V^2(x, y, z, t) + \\ &+ \frac{\partial}{\partial y} \left[D_{\Phi v}(x, y, z, T) \frac{\partial \Phi_{v_1}(x, y, z, t)}{\partial y} \right] + \frac{\partial}{\partial z} \left[D_{\Phi v}(x, y, z, T) \frac{\partial \Phi_{v_1}(x, y, z, t)}{\partial z} \right] - \\ &- k_v(x, y, z, T) V(x, y, z, t). \end{aligned}$$

Integration of left and right sides of Eqs. (8)-(10) on time gives us possibility to obtain relations for the second-order approximations of the required concentrations in the final form

$$\begin{aligned} C_2(x, y, z, t) &= \frac{\partial}{\partial x} \left(\int_0^t D_L(x, y, z, T) \left[1 + \zeta_1 \frac{V(x, y, z, \tau)}{V^*} + \zeta_2 \frac{V^2(x, y, z, \tau)}{(V^*)^2} \right] \frac{\partial C_1(x, y, z, \tau)}{\partial x} \times \right. \\ &\times \left. \left\{ 1 + \xi \frac{[\alpha_{2c} + C_1(x, y, z, \tau)]^\gamma}{P^\gamma(x, y, z, T)} \right\} \right) d\tau + \frac{\partial}{\partial y} \left(\int_0^t \left[1 + \zeta_1 \frac{V(x, y, z, \tau)}{V^*} + \zeta_2 \frac{V^2(x, y, z, \tau)}{(V^*)^2} \right] \times \right. \\ &\times D_L(x, y, z, T) \left. \left\{ 1 + \xi \frac{[\alpha_{2c} + C_1(x, y, z, \tau)]^\gamma}{P^\gamma(x, y, z, T)} \right\} \frac{\partial C_1(x, y, z, \tau)}{\partial y} d\tau \right) + \frac{\partial}{\partial z} \left(\int_0^t \frac{\partial C_1(x, y, z, \tau)}{\partial z} \times \right. \\ &\times D_L(x, y, z, T) \left. \left[1 + \zeta_1 \frac{V(x, y, z, \tau)}{V^*} + \zeta_2 \frac{V^2(x, y, z, \tau)}{(V^*)^2} \right] d\tau \right) + f_c(x, y, z) \end{aligned} \quad (8a)$$

$$\begin{aligned} I_2(x, y, z, t) &= \frac{\partial}{\partial x} \left[\int_0^t D_I(x, y, z, T) \frac{\partial I_1(x, y, z, \tau)}{\partial x} d\tau \right] + \frac{\partial}{\partial y} \left[\int_0^t D_I(x, y, z, T) \frac{\partial I_1(x, y, z, \tau)}{\partial y} d\tau \right] + \\ &+ \frac{\partial}{\partial z} \left[\int_0^t D_I(x, y, z, T) \frac{\partial I_1(x, y, z, \tau)}{\partial z} d\tau \right] - \int_0^t k_{I,I}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, \tau)]^2 d\tau - \\ &- \int_0^t k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, \tau)] [\alpha_{2V} + V_1(x, y, z, \tau)] d\tau + f_I(x, y, z) \end{aligned} \quad (9a)$$

$$\begin{aligned} V_2(x, y, z, t) &= \frac{\partial}{\partial x} \left[\int_0^t D_V(x, y, z, T) \frac{\partial V_1(x, y, z, \tau)}{\partial x} d\tau \right] + \frac{\partial}{\partial y} \left[\int_0^t D_V(x, y, z, T) \frac{\partial V_1(x, y, z, \tau)}{\partial y} d\tau \right] + \\ &+ \frac{\partial}{\partial z} \left[\int_0^t D_V(x, y, z, T) \frac{\partial V_1(x, y, z, \tau)}{\partial z} d\tau \right] - \int_0^t k_{V,V}(x, y, z, T) [\alpha_{2V} + V_1(x, y, z, \tau)]^2 d\tau - \\ &- \int_0^t k_{I,V}(x, y, z, T) [\alpha_{2I} + I_1(x, y, z, \tau)] [\alpha_{2V} + V_1(x, y, z, \tau)] d\tau + f_V(x, y, z) \\ \Phi_{I2}(x, y, z, t) &= \frac{\partial}{\partial x} \left[\int_0^t D_{\Phi I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, \tau)}{\partial x} d\tau \right] - \int_0^t k_I(x, y, z, T) I(x, y, z, \tau) d\tau + \\ &+ \frac{\partial}{\partial y} \left[\int_0^t D_{\Phi I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, \tau)}{\partial y} d\tau \right] + \frac{\partial}{\partial z} \left[\int_0^t D_{\Phi I}(x, y, z, T) \frac{\partial \Phi_{I1}(x, y, z, \tau)}{\partial z} d\tau \right] + \\ &+ \int_0^t k_{I,I}(x, y, z, T) I^2(x, y, z, \tau) d\tau + f_{\Phi I}(x, y, z) \end{aligned} \quad (10a)$$

$$\begin{aligned} \Phi_{V_2}(x, y, z, t) = & \frac{\partial}{\partial x} \left[\int_0^t D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V_1}(x, y, z, \tau)}{\partial x} d\tau \right] - \int_0^t k_V(x, y, z, T) V(x, y, z, \tau) d\tau + \\ & + \frac{\partial}{\partial y} \left[\int_0^t D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V_1}(x, y, z, \tau)}{\partial y} d\tau \right] + \frac{\partial}{\partial z} \left[\int_0^t D_{\Phi_V}(x, y, z, T) \frac{\partial \Phi_{V_1}(x, y, z, \tau)}{\partial z} d\tau \right] + \\ & + \int_0^t k_{V,V}(x, y, z, T) V^2(x, y, z, \tau) d\tau + f_{\Phi_V}(x, y, z). \end{aligned}$$

We determine average values of the second-orders approximations of the required functions by the standard relation [15,16]

$$\alpha_{2\rho} = \frac{1}{\Theta L_x L_y L_z} \int_0^{\Theta} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} [\rho_2(x, y, z, t) - \rho_1(x, y, z, t)] dz dy dx dt. \quad (11)$$

Substitution of the relations (8a)-(10a) into the relation (11) gives us possibility to obtain relations for the required average values $\alpha_{2\rho}$

$$\alpha_{2C} = \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_C(x, y, z) dz dy dx, \quad (12)$$

$$\begin{aligned} \alpha_{2I} = & \frac{1}{2A_{II00}} \left\{ (1 + A_{IV01} + A_{II10} + \alpha_{2V} A_{IV00})^2 - 4A_{II00} [\alpha_{2V} A_{IV10} - A_{II20} + A_{IV11} - \right. \\ & \left. - \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx \right\}^{\frac{1}{2}} - \frac{1 + A_{IV01} + A_{II10} + \alpha_{2V} A_{IV00}}{2A_{II00}}, \quad (13) \end{aligned}$$

$$\alpha_{2V} = \frac{1}{2B_4} \sqrt{\frac{(B_3 + A)^2}{4} - 4B_4 \left(y + \frac{B_3 y - B_1}{A} \right) - \frac{B_3 + A}{4B_4}}.$$

Parameters A_{abij} and other parameters in the relations (13) are presented in the Appendix. Parameters α_{abij} and other parameters in the relations (13) could be written as

$$\begin{aligned} \alpha_{2\Phi_I} = & A_{II20} - \frac{1}{\Theta L_x L_y L_z} \int_0^{\Theta} (\Theta - t) \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} k_I(x, y, z, T) I(x, y, z, t) dz dy dx dt + \\ & + \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_{\Phi_I}(x, y, z) dz dy dx \quad (14) \end{aligned}$$

$$\begin{aligned} \alpha_{2\Phi_V} = & A_{VV20} - \frac{1}{\Theta L_x L_y L_z} \int_0^{\Theta} (\Theta - t) \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} k_V(x, y, z, T) V(x, y, z, t) dz dy dx dt + \\ & + \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_{\Phi_V}(x, y, z) dz dy dx. \end{aligned}$$

The considered substitution gives us possibility to obtain equation for parameter α_{2C} . Solution of the equation depends on value of parameter γ . Analysis of spatio-temporal distributions of concentrations of dopant and radiation defects has been done by using their second-order approximations framework method of averaging of function corrections with decreased quantity of iterative

steps. The second-order approximation is usually a sufficient approximation to obtain qualitative and some quantitative results. Results of analytical modeling have been checked numerically.

3. DISCUSSION

By using the calculated in the previous section relations we analyzed dynamic of redistribution of dopant with account redistribution of radiation defects. Figs. 2 show typical distributions of concentrations of infused and implanted dopants for this case, when dopant diffusion coefficient in the epitaxial layer is larger, than in the substrate. The figures show, that interface between materials gives a possibility to increase sharpness of $p-n$ -junction and at the same time to increase homogeneity of concentration of dopant in doped area.

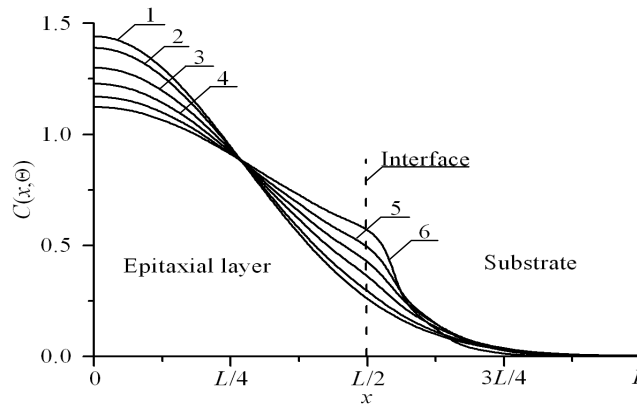


Fig. 2a. Distributions of concentrations of infused dopant in heterostructure from Fig. 1 in direction, which is perpendicular to interface between layers of heterostructure. Increasing of number of curves corresponds to increasing of difference between values of dopant diffusion coefficient in layers of heterostructure. The curves have been calculated under condition, when dopant diffusion coefficient in doped layer is larger, than in nearest layer

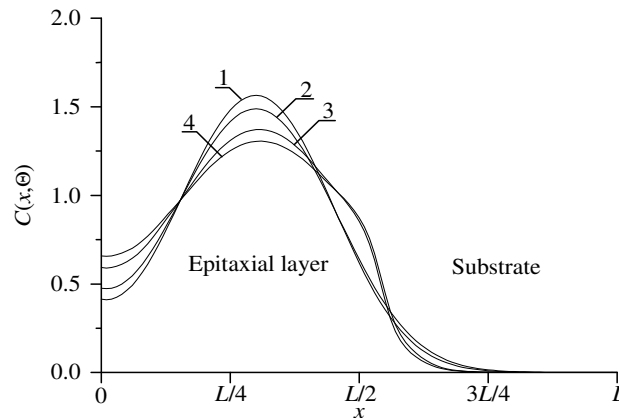


Fig. 2b. Spatial distributions of implanted dopant concentration after annealing. Curves 1 and 2 are calculated distributions of dopant concentration in homogenous structure for two values of annealing time. Curves 3 and 4 are calculated distributions of dopant concentration in heterostructure for the same values of annealing time under condition, when dopant diffusion coefficient in doped layer is larger, than in nearest layer

It is known, that increasing of annealing time leads to increasing of diffusion length into nearest materials of heterostructure. Decrease of annealing time does not allow to fully doped section of the epitaxial layer. We determine compromise annealing time framework recently introduced criterion [17-22]. Framework the criterion we approximate real distribution of concentration of dopant by the step-wise function $\psi(x,y,z)$ (see Figs. 3)

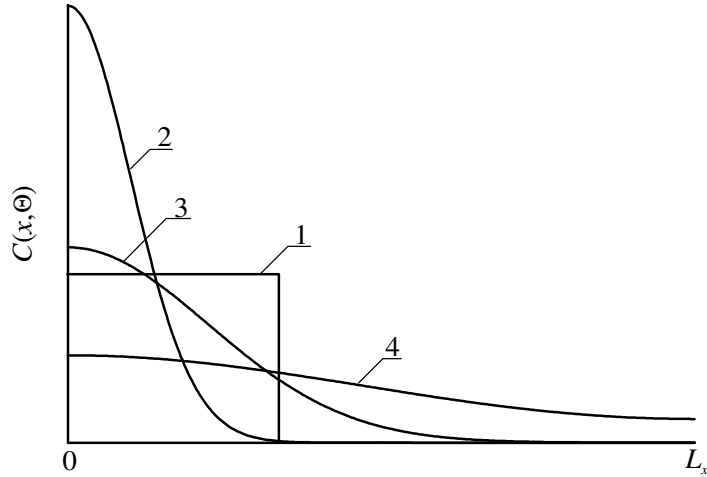


Fig.3a. Spatial distributions of concentration of implanted dopant in heterostructure from Fig. 1. Curve 1 is the idealized distribution of dopant. Curves 2-4 are the real distributions of dopant for different values of annealing time. Increasing of number of curve corresponds to increasing of annealing time

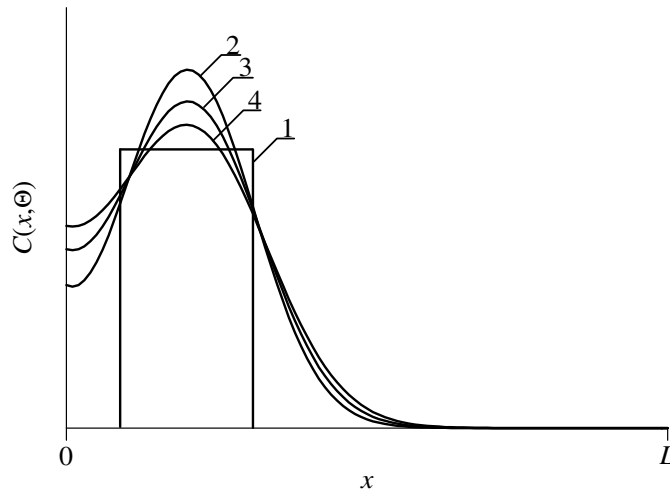


Fig.3b. Spatial distributions of concentration of infused dopant in heterostructure from Fig. 1. Curve 1 is the idealized distribution of dopant. Curves 2-4 are the real distributions of dopant for different values of annealing time. Increasing of number of curve corresponds to increasing of annealing time

$$U = \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} [C(x, y, z, \Theta) - \psi(x, y, z)] dz dy dx. \quad (15)$$

Distributions of concentrations of dopants in Figs. 2 corresponds exactly to compromise annealing time. It should be noted, that presents of interface between layers of heterostructure gives us possibility to manufacture more thin heterotransistor.

4. CONCLUSIONS

In this paper we introduce an approach to manufacture double-base heterotransistor. Several recommendations for optimization of diffusion and ion types of doping to decrease dimensions of double-base heterotransistor have been formulated.

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APPENDIX

$$A_{abij} = \frac{1}{\Theta L_x L_y L_z} \int_0^\Theta (\Theta - t) \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} k_{a,b}(x, y, z, T) I_1^i(x, y, z, t) V_1^j(x, y, z, t) dz dy dx dt,$$

$$B_4 = A_{IV00}^2 A_{IV00}^2 - 2(A_{IV00}^2 - A_{II00} A_{VV00})^2, \quad B_3 = A_{IV00} A_{IV00}^2 + A_{IV01} A_{IV00}^3 + A_{IV00} A_{II10} A_{IV00}^2 -$$

$$- 4(A_{IV00}^2 - A_{II00} A_{VV00}) [2A_{IV01} A_{IV00} + 2A_{IV00} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{IV10} + A_{VV10} + 1)] -$$

$$- 4A_{IV10} A_{IV10} A_{II00} A_{IV00}^2 + 2A_{IV00} A_{IV01} A_{IV00}^2, \quad B_2 = A_{IV00}^2 \{ (1 + A_{IV01} + A_{II10})^2 + A_{IV00}^2 A_{IV01}^2 - A_{II00} \times$$

$$\times 4 \left[A_{IV11} - A_{II20} - \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx \right] + 2A_{IV00} A_{IV01} (A_{IV00} + A_{IV00} A_{IV01} +$$

$$+ A_{IV00} A_{II10} - 4A_{IV10} A_{II00}) \} [2A_{IV01} A_{IV00} + 2A_{IV00} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{IV10} + A_{VV10} +$$

$$+ 1)]^2 + 2 \left[A_{IV01} (1 + A_{IV01} + A_{II10}) + \frac{2}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_V(x, y, z) dz dy dx - 2(A_{VV20} - A_{IV11}) \times$$

$$\times A_{II00} + A_{IV01} (1 + A_{IV01} + A_{II10}) \right] [2A_{IV00} (1 + A_{IV01} + A_{II10}) - 2A_{II00} (A_{IV10} + A_{VV10} + 1) +$$

$$\begin{aligned}
 & + 2A_{IV01}A_{IV00} \Big] \Big\}, B_1 = 2A_{IV00}A_{IV01}(1 + A_{IV01} + A_{II10})^2 - 8A_{IV00}A_{IV01}A_{II00} [A_{IV11} - A_{II20} - \\
 & - \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx \Big] + (A_{IV00} + A_{IV00}A_{IV01} + A_{IV00}A_{II10} - 4A_{IV10}A_{II00}) \times \\
 & \times A_{IV01}^2 - 2 \left[\frac{2A_{II00}}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx + A_{IV01}(1 + A_{IV01} + A_{II10}) - (A_{VV20} - A_{IV11}) \times \right. \\
 & \times 2A_{II00} + A_{IV01}(1 + A_{IV01} + A_{II10}) \Big] [2A_{IV00}(1 + A_{IV01} + A_{II10}) - 2A_{II00}(A_{IV10} + A_{VV10} + 1) + \\
 & + 2A_{IV01}A_{IV00}], B_0 = 4A_{II00}A_{IV01}^2 \left[A_{II20} + \frac{1}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_I(x, y, z) dz dy dx - A_{IV11} \right] - \\
 & - \left[\frac{2A_{II00}}{L_x L_y L_z} \int_0^{L_x} \int_0^{L_y} \int_0^{L_z} f_V(x, y, z) dz dy dx + A_{IV01}(1 + A_{IV01} + A_{II10}) - 2A_{II00}(A_{VV20} - A_{IV11}) + \right. \\
 & \left. + A_{IV01}(1 + A_{IV01} + A_{II10}) \right]^2 + A_{IV01}^2 (A_{IV01} + A_{II10} + 1)^2, y = \sqrt[3]{\sqrt{q^2 + p^3} - q} + B_2/6 - \\
 & - \sqrt[3]{\sqrt{q^2 + p^3} + q}, q = \frac{1}{8} \left[\frac{B_2^3}{27} + B_0(4B_2 - B_3) - B_1^2 + \frac{B_2}{6}(2B_1B_3 - 8B_0) \right], A = \sqrt{8y + B_3^2 - 4B_2}, \\
 & p = [3(2B_1B_3 - 8B_0) - 2B_2^2]/72.
 \end{aligned}$$